

Natural Frequencies and Mode Shapes for Vibrations of Rectangular and Circular Membranes: A Numerical Study

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Abstract— The main goal of present study is to simulate vibrations of rectangular and circular membranes using COMSOL software. In the simulation procedure, two rectangular and one circular membranes with constant thickness have been modeled in COMSOL software. For rectangular and circular membranes, external edges along the perimeter considered to be fixed at zero displacement to simulate the boundary conditions as the Dirichlet boundary conditions. Then natural frequencies and mode shapes are obtained by considering an initial displacement, for simulated membranes. In order to validate the results, two-dimensional wave equation solved for rectangular membranes by considering the Dirichlet boundary conditions. Natural frequencies are derived from the wave equation analytically and are consistent with COMSOL simulations with less than 1% difference.

Keywords— Natural Frequencies, Vibrations of Membranes, COMSOL software.

I. INTRODUCTION

Engineers and scientists have been trying to solve the constitutive equations which they have derived for their models. In many cases, the constitutive equations include linear or nonlinear partial differential equation (PDEs). [1-14] Solving the linear and nonlinear PDEs is not usually an easy solution and nonlinear coefficients make the PDEs very complicated. COMSOL is a useful cross-platform finite element analysis software designed for different simulation problems such as heat transfer, stress analysis, vibration and so on. [14-22]. ABAQUS software is one of the popular FEM software which has been used for wide range of study. Extracting accurate results in ABAQUS depend on defining the boundary conditions, steps of the solution, type, and size of meshes carefully [22-34]. Handful heat transfer, stress analysis and vibrations studied have been done using available commercial FEM software. Currently, COMSOL is using widely because not only is a user-friendly software but also allows coupling a linear or nonlinear equation to the model. [34-50]

The objective of the present study is to simulate the vibrations of rectangular and circular membranes by using COMSOL software. In the simulation procedure, two rectangular and one circular membranes have been modeled for extracting the natural frequencies and mode shapes during vibrations. Dimensions of the first and second rectangles are 4 by 2 ft. and 4 by 3 ft. respectively. To defining the Dirichlet boundary condition, external edges along the perimeter

considered to be fixed at zero displacement. Then response of each rectangular membrane subjected to a given initial displacement condition obtained. For validation purposes, two-dimensional wave equation solved for rectangular membranes by considering the Dirichlet boundary conditions. Natural Frequencies obtained by the wave equation and COMSOL software have less than 1% discrepancy.

II. VIBRATIONS OF THE 2D RECTANGULAR AND CIRCULAR MEMBRANES

For a rectangular membrane in the x-y plane with a length of L and width of K the wave equation can be written as:

$$\frac{\partial^2 z}{\partial t^2} = C^2 \left(\frac{\partial^2 z}{\partial x^2} + \frac{\partial^2 z}{\partial y^2} \right)$$

To describe the Dirichlet boundary conditions, external edges along the perimeter assumed to be fixed at zero displacement. Moreover, the initial velocity is zero at the onset of the vibration. Boundary conditions for vibrations of a rectangular membrane can be written as: Z(-0, t) = 0

$$Z(x,0,t) = 0$$

$$Z(x,k,t) = 0$$

$$Z(0, y, t) = 0$$

$$Z(L, y, t) = 0$$

$$\frac{\partial Z}{\partial t}(x, y, 0) = 0$$

The solution of the wave equation for the selected boundary conditions is as:

$$Z(x, y, t) = \sum_{n=1}^{\alpha} \sum_{m=1}^{\alpha} a_{nm} \cdot \sin \frac{n \prod x}{L} \sin \frac{m \prod y}{k} \cos(w_{nm}t)$$

where, w_{nm} is the natural frequency and can be written as:

$$w_{nm} = \prod C \cdot \sqrt{\frac{n^2}{L^2} + \frac{m^2}{K^2}}$$

For a circular membrane in the x-y plane with a radius of R, the wave equation can be written in polar coordinates as:

$$\frac{\partial^2 z}{\partial t^2} = C^2 \left(\frac{\partial^2 z}{\partial r^2} + \frac{1}{r} \cdot \frac{\partial z}{\partial \theta} + \frac{1}{r} \cdot \frac{\partial^2 z}{\partial \theta^2} \right)$$

The Dirichlet boundary conditions are defined in a way that external edges along the perimeter of the circle are fixed at zero displacement similar to rectangular membranes. Likewise, the initial velocity presumed to be zero at t=0. The



boundary conditions for vibrations of a circular membrane can be written as:

$$Z(R,t) = 0$$
$$\frac{\partial Z}{\partial t}(r,0) = 0$$

The solution to the wave equation for the selected boundary conditions is as:

$$Z(r,t) = \sum_{n=1}^{\alpha} a_n J_0\left(\frac{J_n r}{R}\right) \cdot \cos\left(\frac{J_n C}{R}t\right)$$

III. RESULTS OF NATURAL FREQUENCIES AND MODE SHAPES FOR VIBRATIONS OF RECTANGULAR AND CIRCULAR MEMBRANES

In this study, two rectangular and one circular membranes have been modeled for extracting the natural frequencies and mode shapes under vibrations. Dimensions of the first rectangle selected as 4 by 2 ft. Wave equation and boundary condition for the first rectangular membrane is as follows:

$$\frac{\partial^2 Z}{\partial t^2} = 25 \cdot \left(\frac{\partial^2 z}{\partial x^2} + \frac{\partial^2 z}{\partial y^2} \right)$$

$$Z(x, y, 0) = 0 \cdot 1(4x - x^2) \cdot (2y - y^2))$$

$$\frac{\partial Z}{\partial t}(x, y, 0) = 0$$

Figure 1 shows natural frequencies and mode shapes for vibrations of the first rectangular membrane.

Table 1 demonstrates a comparison between the analytical solution of the PDE and COMSOL results for the natural frequencies of the first rectangular membrane.

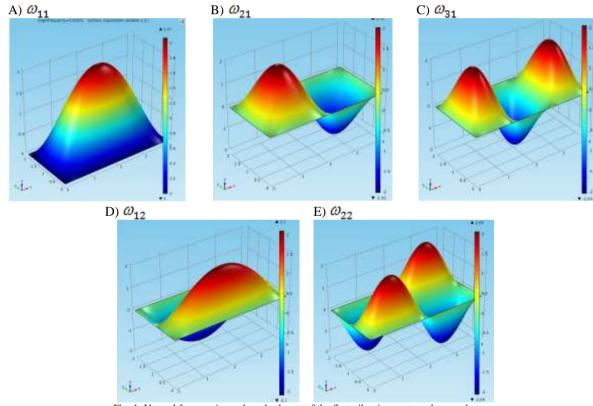


Fig. 1. Natural frequencies and mode shapes of the first vibrating rectangular membrane.

TABLE 1. Comparison between the analytical solution of the PDE and COMSOL results

NATURAL FREQUENCIES	COMSOL	PDE	DIFFERENCE (%)
ω ₁₁	1.25002π	1.25 π	0.0016
ω ₂₁	1.5812 π	1.5811 π	0.0063
ω ₃₁	2.0158 π	2.01556 π	0.0119
ω ₁₂	2.305 π	2.3048 π	0.0087
ω ₂₂	2.5004 π	2.5 π	0.0160

Dimensions of the second rectangle are 4 by 3 ft. Wave equation and boundary condition for the second rectangular membrane is as follow:

$$\frac{\partial^2 Z}{\partial t^2} = 8 \cdot \left(\frac{\partial^2 z}{\partial x^2} + \frac{\partial^2 z}{\partial y^2} \right)$$
$$Z(x, y, 0) = 0 \cdot 1(4x - x^2) \cdot (3y - y^2)$$
$$\frac{\partial Z}{\partial t}(x, y, 0) = 0$$

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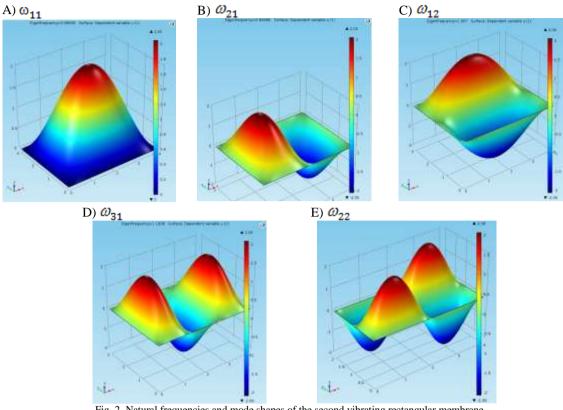


Fig. 2. Natural frequencies and mode shapes of the second vibrating rectangular membrane.

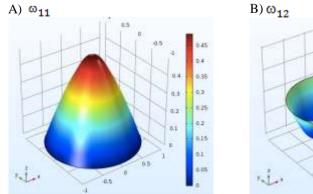
Figure 2 shows natural frequencies and mode shapes for vibrations of the second rectangular membrane.

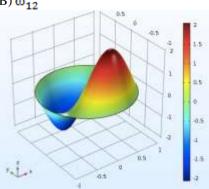
Table 2 illustrates a comparison between the analytical solution of the PDE and COMSOL results for natural frequencies of the second rectangular membrane.

Finally, as it can be seen, Figure 3 shows the results of studying the vibrations of circular membranes to determine frequencies and mode shapes.

TABLE 2. the Analytical and simulation results of the second vibrating rectangular membrane

NATURAL FREQUENCIES	COMSOL	PDE	DIFFERENCE (%)
ω ₁₁	1.17852π	1.17833 π	0.0161
0 ₂₁	1.69972 π	1.69941 π	0.0182
00 ₃₁	2.014 π	2.01356π	0.0218
00 ₁₂	2.3216 π	2.321 π	0.0258
00 ₂₂	2.3572 π	2.3566 π	0.0255





32

Navid Namdari and Amir Dehghan, "Natural frequencies and mode shapes for vibrations of rectangular and circular membranes: A numerical study," International Research Journal of Advanced Engineering and Science, Volume 3, Issue 2, pp. 30-34, 2018.



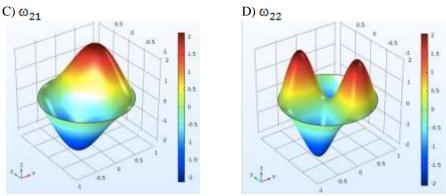


Fig. 3. Natural frequencies and mode shapes for vibration of the circular membrane.

IV. CONCLUSION

COMSOL software is a user-friendly finite element analysis package that can be used to solve linear or nonlinear partial differential equations (PDEs) in different areas such as heat transfer, stress analysis, and vibrations. In the present study, two rectangular and one circular membranes are modeled in order to extract the natural frequencies and mode shapes during the vibrations. For validation purposes, twodimensional wave equation solved for rectangular membranes by considering the Dirichlett boundary conditions. Natural Frequencies obtained from the wave equations and COMSOL are in a very good agreement with less than 1% difference that shows the accuracy of COMSOL solutions.

REFERENCE

- R. Benamar, M.M.K Bennouna, and R.G. White." The effect of large vibration amplitudes on the mode shapes and natural frequencies of thin elastic structures. Part III: Fully Clamped Isotropic Rectangular plate. Measurements of the mode shape amplitude dependence of the spatial distribution of harmonic distortion," *Journal of Sound and Vibration*, vol. 175, issue 3, pp. 377-395, 1994.
- [2] H. Zamanian, M. Salehi, "Modification to Heywood's equations to estimate the stress concentration factors for unidirectional glass epoxy laminates with circular and square holes," *International Research Journal* of Advanced Engineering and Science, vol. 1, issue 4, pp. 18-25, 2016.
- [3] H. Zamanian, F. Javidpour, "Dynamic modeling, and simulation of 4-Wheel skid-steering mobile robot with considering tires longitudinal and lateral slips". *International Journal of Scientific Research in Knowledge*, vol. 4, no 2, pp. 040-55, 2016.
- [4] A. Franco, "An analytical method for the optimum thermal design of convective longitudinal fin arrays," *Heat and Mass Transfer*, vol. 45, no. 12, pp. 1503–1517, 2009.
- [5] S. Timoshenko, Young DH, Vibration Problems in Engineering, ed. 3rd., New York, NY: D. Van Nostrand Co., Inc, pp. 439–440, 1955.
- [6] E. S. Leland, P. K. Wright. "Resonance tuning of piezoelectric vibration energy scavenging generators using compressive axial preload". *Smart Mater Struct*, vol. 15, pp. 1413–1420, 2006.
- [7] W. W. Lin and D. J. Lee, "Boiling on a straight pin fin with variable thermal conductivity," *Heat and Mass Transfer*, vol. 34, no. 5, pp. 381– 386, 1999.
- [8] K. Kalinova, "Influence of nanofibrous membrane configuration on the sound absorption coefficient and resonant frequency," in *Proceedings of* the 6th AUTEX World Textile Conference, Raleigh, NC, USA, 2006.
- [9] J. Rehder, P. Rombach, and O. Hansen, "Balanced membrane micromachined loudspeaker for hearing instrument application," *Journal* of Micromechanics and Microengineering, vol. 11, no. 4, pp. 334–338, 2001

- [10] S. C. Ko, Y. C. Kim, S. S. Lee, S. H. Choi, and S. R. Kim, "Micromachined piezoelectric membrane acoustic device," Sensors and Actuators A: Physical, vol. 103, no. 1-2, pp. 130–134, 2003.
- [11] L. Tirkkonen, H. Halonen, J. Hyttinen et al., "The effects of vibration loading on adipose stem cell number, viability and differentiation towards bone-forming cells," *Journal of the Royal Society Interface*, vol. 8, no. 65, pp. 1736–1747, 2011.
- [12] K. Sato, "Forced vibration analysis of a composite rectangular membrane consisting of strips," *Journal of Sound and Vibration*, vol. 63, no. 3, pp. 411–417, 1979.
- [13] L. Bauer and E. L. Reiss, "Free vibrations of rhombic plates and membranes," *The Journal of the Acoustical Society of America*, vol. 54, no. 5, pp. 1373–1375, 1973
- [14] Q. G. Xu, J. H. Su, D. J. Han et al., "Discussion for several issues of tensioned membrane structure during load analysis," Special Structure, vol. 21, no. 4, pp. 9–12, 2004.
- [15] B. Chen, Y. Wu, and S. Z. Shen, "Wind-induced response analysis of wave-shaped membrane structures," *Spatial Structure*, vol. 10, no. 3, pp. 41–45, 2004.
- [16] H. Zamanian, B. Marzban, P. Bagheri, M. Gudarzi, "On Stress Concentration Factor for Randomly Oriented Discontinuous Fiber Laminas with Circular/Square Hole", *Journal of Science and Engineering*, vol. 3, issue 1, pp. 7-18, 2013.
- [17] H. C. "Unal, "The effect of the boundary at a fin tip on the performance of the fin with and without internal heat generation," *International Journal of Heat and Mass Transfer*, vol. 31, no. 7, pp. 1483–1496, 1998.
- [18] W. M. Murray. "Heat transfer through an annular disk or fin of uniform thickness," Transactions of the American Society of Mechanical Engineers, *Journal of Applied Mechanics*, vol. 60, p. 78, 1938.
- [19] H. Zamanian, M. Kankarani Farahani, A. Assempour. "Initial Blank Design of Deep Drawn Metal Matrix Composites Using Invers Finite Element Method", 20th Annual International Conference on Mechanical Engineering-ISME2012, 2012.
- [20] H. Zamanian, M. Bostan Shirin, and A. Assempour. "Initial blank design of deep drawn orthotropic materials using inverse finite element method". *Journal of Computational & Applied Research in Mechanical Engineering (JCARME)*, vol. 3, issue 2, pp. 125-134, 2014.
- [21] C. Shin, J. Chung, H. H. Yoo. "Dynamic responses of the in-plane and out-of-plane vibrations for an axially moving membrane". *Journal of Sound and Vibration*, vol. 297, pp. 794–809, 2006.
- [22] Zheng Zhou-Lian, Liu Chang-Jiang, He Xiao-Ting, and Chen Shan-Lin, "Free vibration analysis of rectangular orthotropic membranes in large deflection," Hindawi Publishing Corporation Mathematical Problems in Engineering, vol. 2009, Article ID 634362, 9 pages.
- [23] S. Kukathasan and S. Pellegrino, Nonlinear Vibration Of Wrinkled Membranes, University of Cambridge, Cambridge, CB2 1PZ, UK 44th, AIAA 2003-1747;
- [24] M. Ghobadnam, P. Mosaddegh, N. Namdari, M. Masoomi, and A. Ghaei. "Thermo-mechanical characterization of high impact polystyrene sheets using uniaxial stress relaxation tests," *The Bi-Annual International Conference on Experimental Solid Mechanics and Dynamics*, 2014.
- [25] H. Zamanian, B. Marzban, M. Gudarzi, S. Amoozegar, "Investigation of the effect of dental implant screw pitch on the stress and strain distribution in the mandibular bone, Amirkabir University of

Navid Namdari and Amir Dehghan, "Natural frequencies and mode shapes for vibrations of rectangular and circular membranes: A numerical study," *International Research Journal of Advanced Engineering and Science*, Volume 3, Issue 2, pp. 30-34, 2018.

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technology," 19th Iranian Conference of Biomedical Engineering (ICBME), 2012.

- [26] Vibrations of elastic membranes with moving boundaries, Juan Limaco Ferrela, Luis Adauto Medeiros, Nonlinear Analysis, vol. 45, pp. 363–382, 2001.
- [27] Y. Y. Kim and J. H. Kang, "Free vibration analysis of membranes using wave-type base functions," *The Journal of the Acoustical Society of America*, vol. 99, no. 5, pp. 2938–2946, 1996.
- [28] G. W. Wei, "Vibration analysis by discrete singular convolution," *Journal of Sound and Vibration*, vol. 244, no. 3, pp. 535–553, 2001.
- [29] V. H. Cortinez and P. A. A. Laura, "Vibrations of non-homogeneous rectangular membranes," *Journal of Sound and Vibration*, vol. 156, no. 2, pp. 217–225, 1992.
- [30] C. P. Filipich and M. B. Rosales, "Vibration of non-homogeneous rectangular membranes with arbitrary interfaces," *Journal of Sound and Vibration*, vol. 305, no. 4-5, pp. 582–595, 2007.
- [31]K. F. Kolsti and D. L. Kunz, "A point collocation method for geometrically nonlinear membranes," *International Journal of Solids and Structures*, vol. 50, no. 2, pp. 288–296, 2013.
- [32] C. H. M. Jenkins and U. A. Korde, "Membrane vibration experiments: an historical review and recent results," *Journal of Sound and Vibration*, vol. 295, no. 3–5, pp. 602–613, 2006.
- [33] P. A. A. Laura, R. E. Rossi, and R. H. Gutierrez, "The fundamental frequency of non-homogeneous rectangular membranes," *Journal of Sound and Vibration*, vol. 204, no. 2, pp. 373–376, 1997.
- [34] S. H. Ho and C. K. Chen, "Free vibration analysis of non-homogeneous rectangular membranes using a hybrid method," *Journal of Sound and Vibration*, vol. 233, no. 3, pp. 547–555, 2000.
- [35] R. G. Bacabac, T. H. Smit, J. J. W. A. Van Loon, B. Z. Doulabi, M. Helder, and J. Klein-Nulend, "Bone cell responses to high-frequency vibration stress: does the nucleus oscillate within the cytoplasm?" *The FASEB Journal*, vol. 20, no. 7, pp. 858–864, 2006.
- [36] W. X. Wu, C. Shu, and C. M. Wang, "Vibration analysis of arbitrarily shaped membranes using local radial basis function-based differential quadrature method," *Journal of Sound and Vibration*, vol. 306, no. 1-2, pp. 252–270, 2007.
- [37] A. Alsahlani and R. Mukherjee, "Dynamics of a circular membrane with an eccentric circular areal constraint: analysis and accurate simulations," *Simulation Modelling Practice and Theory*, vol. 31, pp. 149–168, 2012.
- [38] S. Durvasula, "Natural frequencies and modes of skew membranes," *The Journal of the Acoustical Society of America*, vol. 44, no. 6, pp. 1636–1646, 1968.
- [39] Torcasio, G. H. Van Lenthe, and H. Van Oosterwyck, "The importance of loading frequency, rate and vibration for enhancing bone adaptation and implant osseointegration," *European Cells and Materials*, vol. 16, pp. 56–68, 2008.

- [40] C. Zhao and G. P. Steven, "An asymptotic formula for correcting finite element predicted natural frequencies of membrane vibration problems," *Communications in Numerical Methods in Engineering*, vol. 12, no. 1, pp. 63–73, 1996.
- [41] J. Wang, "Nonlinear free vibration of the circular plate with large deflection," *Journal of South China University of Technology*, vol. 29, no. 8, pp. 4–6, 2001.
- [42] M. G. Milsted and J. R. Hutchinson, "Use of trigonometric terms in the finite element method with application to vibrating membranes," *Journal* of Sound and Vibration, vol. 32, no. 3, pp. 327–346, 1974.
- [43] A. Y. T. Leung, B. Zhu, J. Zheng, and H. Yang, "A trapezoidal Fourier pelement for membrane vibrations," *Thin-Walled Structures*, vol. 41, no. 5, pp. 479–491, 2003.
- [44] N. Rosenberg, M. Levy, and M. Francis, "Experimental model for stimulation of cultured human osteoblast-like cells by high frequency vibration," *Cytotechnology*, vol. 39, no. 3, pp. 125–130, 2002.
- [45] T. Shikata, T. Shiraishi, S. Morishita, R. Takeuchi, and T. Saito, "Effects of amplitude and frequency of mechanical vibration stimulation on cultured osteoblasts," *Journal of System Design and Dynamics*, vol. 2, no. 1, pp. 382–388, 2008.
- [46] E. Lau, S. Al-Dujaili, A. Guenther, D. Liu, L. Wang, and L. You, "Effect of low-magnitude, high-frequency vibration on osteocytes in the regulation of osteoclasts," *Bone*, vol. 46, no. 6, pp. 1508–1515, 2010.
- [47] B. R. Beck, "Vibration therapy to prevent bone loss and falls: mechanisms and efficacy," *Current Osteoporosis Reports*, vol. 13, no. 6, pp. 381–389, 2015.
- [48] [45] A. Houmat, "Free vibration analysis of arbitrarily shaped membranes using the trigonometric p-version of the finite-element method," *Thin-Walled Structures*, vol. 44, no. 9, pp. 943–951, 2006
- [49] W. H. Wittrick and F. W. Williams, "A general algorithm for computing natural frequencies of elastic structures," *The Quarterly Journal of Mechanics and Applied Mathematics*, vol. 24, no. 3, pp. 263–284, 1971
- [50] D. A. Vega, S. A. Vera, and P. A. A. Laura, "Fundamental frequency of vibration of rectangular membranes with an internal oblique support," *Journal of Sound and Vibration*, vol. 224, no. 4, pp. 780–783, 1999.
- [51] U. Lee, Spectral Element Method in Structural Dynamics, John Wiley & Sons, Singapore, 2009.
- [52] W. H. Wittrick and F. W. Williams, "A general algorithm for computing natural frequencies of elastic structures," *The Quarterly Journal of Mechanics and Applied Mathematics*, vol. 24, no. 3, pp. 263–284, 1971.
- Mechanics and Applied Mathematics, vol. 24, no. 3, pp. 263–284, 1971.
 [53] H. Ersoy, Ö. Civalekb, and L. Özpolatb, "Free vibration analysis of rectangular membranes with variable density using the discrete singular convolution approach," Asian Journal of Civil Engineering, vol. 11, no. 1, pp. 83–94, 2010.